

By Mustafa Shiple

## Inverse of Transfornnation



## In lnverse of Transfornnation

$$
\begin{aligned}
{ }^{U} T_{E}={ }^{U} T_{R}{ }^{R} T_{H}{ }^{H} T_{E} & ={ }^{U} T_{P}{ }^{P} T_{E} \\
{\left[{ }^{U} T_{R}\right]^{-1}\left[{ }^{U} T_{R}{ }^{R} T_{H}{ }^{H} T_{E}\right]\left[{ }^{H} T_{E}\right]^{-1} } & =\left[{ }^{U} T_{R}\right]^{-1}\left[{ }^{U} T_{P}{ }^{P} T_{E}\right]\left[{ }^{H} T_{E}\right]^{-1} \\
{ }^{R} T_{H} & ={ }^{U} T_{R}{ }^{-1 U} T_{P}{ }^{P} T_{E}{ }^{H} T_{E}{ }^{-1} \\
& ={ }^{R} T_{U}{ }^{U} T_{P}{ }^{P} T_{E}{ }^{E} T_{H}
\end{aligned}
$$

## Inverse matrix

$$
\left[\begin{array}{ll}
a & b \\
c & d
\end{array}\right]^{-1}=\underset{\text { determinant }}{\frac{1}{a d-b c}}\left[\begin{array}{cc}
d & -b \\
-c & a
\end{array}\right]
$$

Pythagorean Trigonometric


## Orthogonal matrices

$$
\begin{aligned}
& {\left[\begin{array}{l}
X_{2} \\
Y_{2}
\end{array}\right]=\left[\begin{array}{cc}
\cos (\alpha) & -\sin (\alpha) \\
\sin (\alpha) & \cos (\alpha)
\end{array}\right]\left[\begin{array}{l}
X_{1} \\
Y_{1}
\end{array}\right]} \\
& {\left[\begin{array}{l}
X_{2} \\
Y_{2}
\end{array}\right]\left[\begin{array}{cc}
\cos (\alpha) & -\sin (\alpha) \\
\sin (\alpha) & \cos (\alpha)
\end{array}\right]^{-1}=\left[\begin{array}{l}
X_{1} \\
Y_{1}
\end{array}\right]}
\end{aligned}
$$

$$
\therefore\left[\begin{array}{cc}
\cos (\alpha) & -\sin (\alpha) \\
\sin (\alpha) & \cos (\alpha)
\end{array}\right]^{-1}=\frac{1}{c^{2}(\alpha)+s^{2}(\alpha)}\left[\begin{array}{cc}
\cos (\alpha) & \sin (\alpha) \\
-\sin (\alpha) & \cos (\alpha)
\end{array}\right]
$$

$$
=\left[\begin{array}{cc}
\cos (\alpha) & \sin (\alpha) \\
-\sin (\alpha) & \cos (\alpha)
\end{array}\right]=G_{R_{L}}{ }^{T}
$$

$$
G_{R_{L}}{ }^{-1}=G_{R_{L}}{ }^{T} \text { Orthogonal matrix }
$$

## Quick Math Review (Dot Product)

$$
=\left[\begin{array}{cc}
\cos (\alpha) & \sin (\alpha) \\
-\sin (\alpha) & \cos (\alpha)
\end{array}\right]=G_{R_{L}}{ }^{T}
$$

Local : $\left[\begin{array}{l}X_{1} \\ Y_{1} \\ Z_{1}\end{array}\right]=\left[\begin{array}{ccc}\cos (\alpha) & \sin (\alpha) & 0 \\ -\sin (\alpha) & \cos (\alpha) & 0 \\ 0 & 0 & 1\end{array}\right]\left[\begin{array}{l}X_{2} \\ Y_{2} \\ Z_{2}\end{array}\right] \uparrow$

## Summary

$$
\begin{array}{ll}
\text { Global : } & {\left[\begin{array}{l}
X_{2} \\
Y_{2} \\
Z_{2}
\end{array}\right]=\left[\begin{array}{ccc}
1 & 0 & 0 \\
0 & \cos (\gamma) & -\sin (\gamma) \\
0 & \sin (\gamma) & \cos (\gamma)
\end{array}\right]\left[\begin{array}{l}
X_{1} \\
Y_{1} \\
Z_{1}
\end{array}\right]} \\
\text { Local : } & {\left[\begin{array}{l}
X_{1} \\
Y_{1} \\
Z_{1}
\end{array}\right]=\left[\begin{array}{ccc}
1 & 0 & 0 \\
0 & \cos (\gamma) & \sin (\gamma) \\
0 & -\sin (\gamma) & \cos (\gamma)
\end{array}\right]\left[\begin{array}{l}
X_{2} \\
Y_{2} \\
Z_{2}
\end{array}\right]}
\end{array}
$$

$$
\text { Global : }\left[\begin{array}{c}
X_{2} \\
Y_{2} \\
Z_{2}
\end{array}\right]=\left[\begin{array}{ccc}
\cos (\beta) & 0 & \sin (\beta) \\
0 & 1 & 0 \\
-\sin (\beta) & 0 & \cos (\beta)
\end{array}\right]\left[\begin{array}{l}
X_{1} \\
Y_{1} \\
Z_{1}
\end{array}\right] \quad \text { Global : }\left[\begin{array}{l}
X_{2} \\
Y_{2} \\
Z_{2}
\end{array}\right]=\left[\begin{array}{ccc}
\cos (\alpha) & -\sin (\alpha) & 0 \\
\sin (\alpha) & \cos (\alpha) & 0 \\
0 & 0 & 1
\end{array}\right]\left[\begin{array}{l}
X_{1} \\
Y_{1} \\
Z_{1}
\end{array}\right]
$$

$$
\left[\begin{array}{l}
X_{1} \\
Y_{1} \\
Z_{1}
\end{array}\right]=\left[\begin{array}{ccc}
\cos (\beta) & 0 & -\sin (\beta) \\
0 & 1 & 0 \\
\sin (\beta) & 0 & \cos (\beta)
\end{array}\right]\left[\begin{array}{l}
X_{2} \\
Y_{2} \\
Z_{2}
\end{array}\right] \quad \text { Local : }\left[\begin{array}{l}
X_{1} \\
Y_{1} \\
Z_{1}
\end{array}\right]=\left[\begin{array}{ccc}
\cos (\alpha) & \sin (\alpha) & 0 \\
-\sin (\alpha) & \cos (\alpha) & 0 \\
0 & 0 & 1
\end{array}\right]\left[\begin{array}{l}
X_{2} \\
Y_{2} \\
Z_{2}
\end{array}\right]
$$

## Properties of a Rotation Matrix

- Example 1

Do the following matrices represent rotation matrices?

$$
\text { a) } R_{1}=\left[\begin{array}{ccc}
-\frac{1}{2} & 0 & -\frac{\sqrt{3}}{2} \\
0 & 1 & 0 \\
-\frac{\sqrt{3}}{2} & 0 & -\frac{1}{2}
\end{array}\right]
$$

b)

$$
R_{2}=\left[\begin{array}{ccc}
-\frac{1}{2} & 0 & -\frac{\sqrt{3}}{2} \\
0 & 1 & 0 \\
\frac{\sqrt{3}}{2} & 0 & -\frac{1}{2}
\end{array}\right]
$$

Solution
a) $\quad \operatorname{det} R_{1}=\frac{1}{2} \quad \Rightarrow$ It is not a rotation matrix
b) $\quad \operatorname{det} R_{2}=1$
$\left.R_{2} R_{2}^{T}=I\right\} \Rightarrow$ It is a rotation matrix

## $4 \times 4$ matrix

$$
T=\left[\begin{array}{cccc}
n_{x} & o_{x} & a_{x} & p_{x} \\
n_{y} & o_{y} & a_{y} & p_{y} \\
n_{z} & o_{z} & a_{z} & p_{z} \\
0 & 0 & 0 & 1
\end{array}\right] \quad \text { and } \quad T^{-1}=\left[\begin{array}{cccc}
n_{x} & n_{y} & n_{z} & -\mathbf{p} \cdot \mathbf{n} \\
o_{x} & o_{y} & o_{z} & -\mathbf{p} \cdot \mathbf{o} \\
a_{x} & a_{y} & a_{z} & -\mathbf{p} \cdot \mathbf{a} \\
0 & 0 & 0 & 1
\end{array}\right]
$$

Emanple:
$T=\left[\begin{array}{cccc}0.5 & 0 & 0.866 & 3 \\ 0.866 & 0 & -0.5 & 2 \\ 0 & 1 & 0 & 5 \\ 0 & 0 & 0 & 1\end{array}\right]$
$T^{-1}=\left[\begin{array}{cccc}0.5 & 0.866 & 0 & -(3 \times 0.5+2 \times 0.866+5 \times 0) \\ 0 & 0 & 1 & -(3 \times 0+2 \times 0+5 \times 1) \\ 0.866 & -0.5 & 0 & -(3 \times 0.866+2 \times-0.5+5 \times 0) \\ 0 & 0 & 0 & 1\end{array}\right]=\left[\begin{array}{cccc}0.5 & 0.866 & 0 & -3.23 \\ 0 & 0 & 1 & -5 \\ 0.866 & -0.5 & 0 & -1.598 \\ 0 & 0 & 0 & 1\end{array}\right]$


## solution

$$
\begin{aligned}
& { }^{R} T_{5} \times{ }^{5} T_{H} \times{ }^{H} T_{E} \times{ }^{E} T_{o b j}={ }^{R} T_{5} \times{ }^{5} T_{c a m} \times{ }^{c a m} T_{o b j} \\
& { }^{5} T_{H} \times{ }^{H} T_{E} \times{ }^{E} T_{o b j}={ }^{5} T_{c a m} \times{ }^{c a m} T_{o b j} \\
& { }^{H} T_{E} \times{ }^{E} T_{o b j}={ }^{5} T_{H}^{-1} \times{ }^{5} T_{c a m} \times{ }^{c a m} T_{o b j} \\
& { }^{E} T_{o b j}={ }^{H} T_{E}{ }^{-1} \times{ }^{5} T_{H}^{-1} \times{ }^{5} T_{c a m} \times{ }^{c a m} T_{o b j} \\
& { }^{E} T_{o b j}={ }^{E} T_{H} \times{ }^{H} T_{5} \times{ }^{5} T_{c a m} \times{ }^{c a m} T_{o b j} \\
& { }^{5} T_{\text {cam }}=\left[\begin{array}{cccc}
0 & 0 & -1 & 3 \\
0 & -1 & 0 & 0 \\
-1 & 0 & 0 & 5 \\
0 & 0 & 0 & 1
\end{array}\right]{ }^{5} T_{H}=\left[\begin{array}{cccc}
0 & -1 & 0 & 0 \\
1 & 0 & 0 & 0 \\
0 & 0 & 1 & 4 \\
0 & 0 & 0 & 1
\end{array}\right]{ }^{c a m} T_{o b j}=\left[\begin{array}{llll}
0 & 0 & 1 & 2 \\
1 & 0 & 0 & 2 \\
0 & 1 & 0 & 4 \\
0 & 0 & 0 & 1
\end{array}\right]{ }^{H} T_{E}=\left[\begin{array}{llll}
1 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 1 & 3 \\
0 & 0 & 0 & 1
\end{array}\right]
\end{aligned}
$$

## solution

$$
{ }^{E} T_{o b j}={ }^{E} T_{H} \times{ }^{H} T_{5} \times{ }^{5} T_{c a m} \times{ }^{c a m} T_{o b j}
$$

$$
{ }^{5} T_{\text {cam }}=\left[\begin{array}{cccc}
0 & 0 & -1 & 3 \\
0 & -1 & 0 & 0 \\
-1 & 0 & 0 & 5 \\
0 & 0 & 0 & 1
\end{array}\right]{ }^{5} T_{H}=\left[\begin{array}{cccc}
0 & -1 & 0 & 0 \\
1 & 0 & 0 & 0 \\
0 & 0 & 1 & 4 \\
0 & 0 & 0 & 1
\end{array}\right]{ }^{\text {cam }} T_{o b j}=\left[\begin{array}{llll}
0 & 0 & 1 & 2 \\
1 & 0 & 0 & 2 \\
0 & 1 & 0 & 4 \\
0 & 0 & 0 & 1
\end{array}\right]{ }^{H} T_{E}=\left[\begin{array}{llll}
1 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 1 & 3 \\
0 & 0 & 0 & 1
\end{array}\right]
$$

$$
\begin{aligned}
{ }^{E} T_{H} & ={ }^{H} T_{E}^{-1}
\end{aligned}=\left[\begin{array}{cccc}
1 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 1 & -3 \\
0 & 0 & 0 & 1
\end{array}\right],\left[\begin{array}{cccc}
0 & 1 & 0 & 0 \\
-1 & 0 & 0 & 0 \\
0 & 0 & 1 & -4 \\
0 & 0 & 0 & 1
\end{array}\right] .
$$

## solution

$$
\begin{aligned}
& { }^{E} T_{o b j}={ }^{E} T_{H} \times{ }^{H} T_{5} \times{ }^{5} T_{c a m} \times{ }^{c a m} T_{o b j} \\
& { }^{5} T_{c a m}=\left[\begin{array}{cccc}
0 & 0 & -1 & 3 \\
0 & -1 & 0 & 0 \\
-1 & 0 & 0 & 5 \\
0 & 0 & 0 & 1
\end{array}\right]{ }^{H} T_{5}=\left[\begin{array}{cccc}
0 & 1 & 0 & 0 \\
-1 & 0 & 0 & 0 \\
0 & 0 & 1 & -4 \\
0 & 0 & 0 & 1
\end{array}\right]{ }^{\text {cam }} T_{o b j}=\left[\begin{array}{llll}
0 & 0 & 1 & 2 \\
1 & 0 & 0 & 2 \\
0 & 1 & 0 & 4 \\
0 & 0 & 0 & 1
\end{array}\right]{ }^{E} T_{H}=\left[\begin{array}{cccc}
1 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 1 & -3 \\
0 & 0 & 0 & 1
\end{array}\right] \\
& { }^{E} T_{o b j}=\left[\begin{array}{cccc}
1 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 1 & -3 \\
0 & 0 & 0 & 1
\end{array}\right]\left[\begin{array}{cccc}
0 & 1 & 0 & 0 \\
-1 & 0 & 0 & 0 \\
0 & 0 & 1 & -4 \\
0 & 0 & 0 & 1
\end{array}\right]\left[\begin{array}{cccc}
0 & 0 & -1 & 3 \\
0 & -1 & 0 & 0 \\
-1 & 0 & 0 & 5 \\
0 & 0 & 0 & 1
\end{array}\right]\left[\begin{array}{llll}
0 & 0 & 1 & 2 \\
1 & 0 & 0 & 2 \\
0 & 1 & 0 & 4 \\
0 & 0 & 0 & 1
\end{array}\right] \\
& =\left[\begin{array}{cccc}
-1 & 0 & 0 & -2 \\
0 & 1 & 0 & 1 \\
0 & 0 & -1 & -4 \\
0 & 0 & 0 & 1
\end{array}\right]
\end{aligned}
$$

## DENAVIT-HARTENBERG REPRESENTATION



- The Denavit-Hartenberg (D-H) method of representation is a very simple way of modeling robot links and joints of any configuration, regardless of the sequence or complexity.
- the direct modeling of robots with the previous techniques is faster and more straight forward.
- D-H representation has an added benefit; analyses of differential motions and Jacobians, dynamic analysis, force analysis, and others are based on the results obtained from D-H representation

Prof.Dick Hartenberg


1950

## Introduction

- Notation: Denavit - Hartenberg = DH
- It describes forward kinematics using 4 parameter for each joint: $\theta_{\mathrm{i}}, d_{\mathrm{i}}, a_{\mathrm{i}}, \alpha_{\mathrm{i}}$

| Artic. $\boldsymbol{i}$ | $d_{\mathrm{i}}$ | $\theta_{\mathrm{i}}$ | $a_{\mathrm{i}}$ | $\alpha_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 450 | $180+q_{1}$ | -150 | 90 |
| 2 | 0 | $90+q_{2}$ | 600 | 0 |
| 3 | 0 | $180+q_{3}$ | -200 | 90 |
| 4 | 640 | $180+q_{4}$ | 0 | 90 |
| 5 | 0 | $180+q_{5}$ | 0 | 90 |
| 6 | 0 | $q_{6}$ | 0 | 0 |

## D-H Procedure

- It is a systematic (and classical) method used to describe forward kinematics of manipulators
- Procedure

1. Determine 1 frame per joint (based on some rules)
2. Determine 4 parameters $\left(\theta_{\mathrm{i}}, d_{\mathrm{i}}, a_{\mathrm{i}}, \alpha_{\mathrm{i}}\right)$ that describe the pose between every two reference frames (based on rules)
3. Using the 4 parameters (per joint) compute the homogeneous transformation matrices
$\rightarrow$ Determine the pose of the end effector with respect to the base (product of the homogeneous transformation matrices)

Step 1: Determine 1 frame per joint (based on some rules)


Joint 3

A. Axis $z_{i}$ : align $z_{i}$ with the axis of motion of joint $i+1$, If the joint is prismatic, the z axis is along the direction of the linear movement.
B. Origin of frame $\{i\}$ : At the intersection of $z_{i} \& z_{i-1}$. Or any point if they are in parallel


## Denavit-Hartenberg Convention

Step 1: Determine 1 frame per joint (based on some rules)
C. Axis $x_{i}$ : assign $x_{i}$ in the direction of $z_{i-1} \times z_{i}$. If $\left(z_{i-1} \& z_{i}\right)$ are parallel, assign $x_{i}$ along the common normal between $z_{i-1} \& z_{i}$
D. Axis $y_{i}$ : assign $\boldsymbol{y}_{i}$ to complete the frame (following the right-hand rule)


## Denavit-Hartenberg Convention

## Step 1: Determine 1 frame per joint (based on some rules)

D. End effector frame $\{n\}$ :

- $\boldsymbol{x}_{n}$ must be orthogonal to $z_{n-1}$ and it must intersect it (the origin of the frame is usually at the end of the kinematic chain)
- Usually $z_{n}$ goes in the same direction as $z_{n-1}$ pointing outwards
- $y_{n}$ completes the frame (right hand rule)



## Denavit-Hartenberg Convention

## (2) Assigning the DH Parameters

## Joint Parameters

- Joint angle $\left(\theta_{i}\right)$ : rotation angle from axis $\boldsymbol{x}_{i-1}$ to axis $\boldsymbol{x}_{i}$ about axis $z_{i-1}$
$\rightarrow$ It is the joint variable if the $i$-th joint is revolute
- Joint displacement $\left(d_{i}\right)$ : distance from the origin of frame $\{i-1\}$ to the intersection of axis $z_{i-1}$ to axis $\boldsymbol{x}_{i}$ along axis $z_{i-1}$
$\rightarrow$ It is the joint variable if the $i$-th joint is prismatic


## Link Parameters (constants)

- Link length $\left(a_{i}\right)$ : distance from the intersection of axis $z_{i-1}$ and axis $\boldsymbol{x}_{i}$ to the origin of frame $\{i\}$ along axis $\boldsymbol{x}_{i}$ (shortest path)
- Link rotation angle $\left(\alpha_{i}\right)$ : rotation angle from axis $z_{i-1}$ to axis $z_{i}$ about axis $\boldsymbol{x}_{i}$


## Denavit-Hartenberg Convention

(2) Assigning the DH Parameters


## Link parameters

- $a_{i}$ : distance from $\left[z_{i+1}\right]$ to $\left[z_{i}\right]$.by drawing a line perpendicular to both $z$ axes
- $\alpha_{i}$ : angle from $z_{i+1}$ to $z_{i}$ about $\boldsymbol{x}_{i}$

Joint $n$
Joint $n+1$
Joint $n+2$


## Denavit-Hartenberg Convention

(2) Assigning the DH Parameters


## Joint parameters

- $d_{i}$ : distance from the origin of $\{i-1\}$ to the [intersection of $z_{i-1}$ with $x_{i}$ ] along $z_{i-1}$
- $\theta_{i}$ : rotation angle from $\boldsymbol{x}_{i-1}$ to $\boldsymbol{x}_{i}$ about $z_{i-1}$


## Denavit-Hartenberg Convention

(2) Assigning the DH Parameters


## Summary

- $d_{i}$ : distance from the origin of $\{i-1\}$ to the [intersection of $z_{i-1}$ with $\boldsymbol{x}_{i}$ ] along $z_{i-1}$
- $\boldsymbol{\theta}_{i}$ : rotation angle from $\boldsymbol{x}_{i-1}$ to $\boldsymbol{x}_{i}$ about $z_{i-1}$
- $a_{i}$ : distance from [the intersection of $z_{i-1}$ with $\boldsymbol{x}_{i}$ ] to the origin of $\{i\}$ along $\boldsymbol{x}_{i}$
- $\alpha_{i}$ : angle from $z_{i-1}$ to $z_{i}$ about $\boldsymbol{x}_{i}$


## Denavit-Hartenberg Reference Frame Layout

Produced by Ethan Tira-Thompson


Denavit-Hartenberg Reference Frame Layout - YouTube

(b)

(e)

(c)

(f)

(d)

(g)

## transformation ${ }^{\mathrm{n}} \mathrm{T}_{\mathrm{n}+1}$

$$
\begin{align*}
& { }^{n} T_{n+1}=A_{n+1}=\operatorname{Rot}\left(z, \theta_{n+1}\right) \times \operatorname{Trans}\left(0,0, d_{n+1}\right) \times \operatorname{Trans}\left(a_{n+1}, 0,0\right) \times \operatorname{Rot}\left(x, \alpha_{n+1}\right) \\
& =\left[\begin{array}{cccc}
C \theta_{n+1} & -S \theta_{n+1} & 0 & 0 \\
S \theta_{n+1} & C \theta_{n+1} & 0 & 0 \\
0 & 0 & 1 & 0 \\
0 & 0 & 0 & 1
\end{array}\right] \times\left[\begin{array}{cccc}
1 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 1 & d_{n+1} \\
0 & 0 & 0 & 1
\end{array}\right] \times\left[\begin{array}{cccc}
1 & 0 & 0 & a_{n+1} \\
0 & 1 & 0 & 0 \\
0 & 0 & 1 & 0 \\
0 & 0 & 0 & 1
\end{array}\right] \times\left[\begin{array}{cccc}
1 & 0 & 0 & 0 \\
0 & C \alpha_{n+1} & -S \alpha_{n+1} & 0 \\
0 & S \alpha_{n+1} & C \alpha_{n+1} & 0 \\
0 & 0 & 0 & 1
\end{array}\right] \\
& A_{n+1}=\left[\begin{array}{cccc}
C \theta_{n+1} & -S \theta_{n+1} C \alpha_{n+1} & S \theta_{n+1} S \alpha_{n+1} & a_{n+1} C \theta_{n+1} \\
S \theta_{n+1} & C \theta_{n+1} C \alpha_{n+1} & -C \theta_{n+1} S \alpha_{n+1} & a_{n+1} S \theta_{n+1} \\
0 & S \alpha_{n+1} & C \alpha_{n+1} & d_{n+1} \\
0 & 0 & 0 & 1
\end{array}\right] \tag{2.53}
\end{align*}
$$

## Example 1: DH of a SCARA Robot

1. Reference frames


- Number joint axis
- Base reference frame: $z_{0}$ along the axis of joint 1 (arbitrary origin, arbitrary $x_{0}$ )


## Example 1: DH of a SCARA Robot

## 1. Reference frames



- Axis $z_{i}: z_{i}$ along the axis of joint $i+1$
- Origin of frame $\{i\}$ :
a) Intersection of $z_{i} \& z_{i-1}$, or
b) Intersection of $z_{i}$ with normal between $z_{i} \& z_{i-1}$ (If $z_{i} \& z_{i-1}$ parallel: arbitrary normal)
- Axis $x_{i}$ : in the direction of $z_{i-1} \times z_{i}$. If $\left(z_{i-1} \& z_{i}\right)$ are parallel, $\boldsymbol{x}_{i}$ along their common normal
- Axis $y_{i}$ : assign $\boldsymbol{y}_{i}$ to complete the frame (using the right hand rule)


## Example 1: DH of a SCARA Robot

## 1. Reference frames



- End effector frame $\{n\}$ :
- $\boldsymbol{x}_{n}$ orthogonal to $z_{n-1}$, intersecting it (origin at the end of the chain)
- $z_{n}$ in the direction of $z_{n-1}$ pointing outwards
- $y_{n}$ completes the frame

Example 1: DH of a SCARA Robot

## 2. DH parameters



| Joint $i$ | $d_{\mathrm{i}}$ | $\theta_{\mathrm{i}}$ | $a_{\mathrm{i}}$ | $a_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 | $l_{1}$ | $180+q_{1}$ | $l_{2}$ | 0 |
| 2 | 0 | $-90+q_{2}$ | $l_{3}$ | 0 |
| 3 | $-l_{4}+q_{3}$ | 0 | 0 | 0 |
| 4 | 0 | $90+q_{4}$ | 0 | 180 |

$d_{i}$ distance from $\{i-1\}$ to [intersection of $z_{i-1}$ with $\left.x_{i}\right]$ along $z_{i-1}$
$\theta_{i}:$ angle from $\boldsymbol{x}_{i-1}$ to $\boldsymbol{x}_{i}$ alrededor de $\boldsymbol{z}_{i-1}$
$a_{i}$ : distance from [intersection of $z_{i-1}$ wtih $x_{i}$ ] to $\{i\}$ along $\boldsymbol{x}_{i}$
$\alpha_{i}$ : angle from $z_{i-1}$ to $z_{i}$ about $\boldsymbol{x}_{i}$

## Example 1: DH of a SCARA Robot

## 3. Homogeneous Transformation Matrices

$$
\begin{aligned}
& \begin{array}{|c|c|c|c|c|}
\hline \text { Jointi } & a_{1} & & a_{1} \\
\hline 1 & l_{1} & 180+q_{1} & l_{2} & 0 \\
\hline 2 & 0 & -90+q_{2} & l_{3} & 0 \\
\hline 3 & -l_{4}+q_{3} & 0 & 0 & 0 \\
\hline 4 & 0 & 90+q_{4} & 0 & 180 \\
\hline
\end{array} \\
& { }^{0} T_{1}\left(q_{1}\right)=\left[\begin{array}{cccc}
-\cos q_{1} & \sin q_{1} & 0 & -l_{2} \cos q_{1} \\
-\sin q_{1} & -\cos q_{1} & 0 & -l_{2} \sin q_{1} \\
0 & 0 & 1 & l_{1} \\
0 & 0 & 0 & 1
\end{array}\right] \quad{ }^{2} T_{3}\left(q_{3}\right)=\left[\begin{array}{cccc}
1 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 1 & q_{3}-l_{4} \\
0 & 0 & 0 & 1
\end{array}\right] \\
& { }^{1} T_{2}\left(q_{2}\right)=\left[\begin{array}{cccc}
\sin q_{2} & \cos q_{2} & 0 & l_{3} \sin q_{2} \\
-\cos q_{2} & \sin q_{2} & 0 & -l_{3} \cos q_{2} \\
0 & 0 & 1 & 0 \\
0 & 0 & 0 & 1
\end{array}\right] \\
& { }^{3} T_{4}\left(q_{4}\right)=\left[\begin{array}{cccc}
-\sin q_{4} & \cos q_{4} & 0 & 0 \\
\cos q_{4} & \sin q_{4} & 0 & 0 \\
0 & 0 & -1 & 0 \\
0 & 0 & 0 & 1
\end{array}\right]
\end{aligned}
$$

## Example 1: DH of a SCARA Robot

## 3. Homogeneous Transformation Matrices

- End effector with respect to the base:

$$
\begin{aligned}
{ }^{0} T_{4} & =\left({ }^{0} T_{1}\right)\left({ }^{1} T_{2}\right)\left({ }^{2} T_{3}\right)\left({ }^{3} T_{4}\right) \\
& =\left[\begin{array}{cccc}
-c_{124} & -s_{124} & 0 & -l_{3} s_{12}-l_{2} c_{1} \\
-s_{124} & c_{124} & 0 & l_{3} c_{12}-l_{2} s_{1} \\
0 & 0 & -1 & l_{1}-l_{4}+q_{3} \\
0 & 0 & 0 & 1
\end{array}\right]
\end{aligned}
$$

- For the initial configuration ( $\left.q_{1}=q_{2}=q_{3}=q_{4}=0\right)$ :

$$
{ }^{0} T_{4}=\left[\begin{array}{cccc}
-1 & 0 & 0 & -l_{2} \\
0 & 1 & 0 & l_{3} \\
0 & 0 & -1 & l_{1}-l_{4} \\
0 & 0 & 0 & 1
\end{array}\right]
$$



Robot in the initial configuration

Compare with the result obtained using the geometric method

THE END


